Department of Radiation Oncology





Argonne National Laboratory Course: 3DCRT for Technologists

CLINICAL DOSIMETRY IN RADIOTHERAPY

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Advertencia:

Spanglish

From Wikipedia, the free encyclopedia

Spanglish — also called espanglish, espaninglish, el spanish broken, inglañol, or espan'glés, a blend of the English-language words for "Spanish" and "English" — is a name used to refer to a range of language-contact phenomena, primarily in the speech of the Hispanic population of the United States, which is exposed to both Spanish and English. These phenomena are a product of close border contacts or large bilingual communities, such as along the United States-Mexico border and throughout Southern California, northern New Mexico, Texas, Florida, <u>Puerto Rico</u>, and in New York City.

Dose Ratios and MU Calculations



Not as *scary* as you think!

Our Goals:

- A. Actually understand things like PDDs, Inverse Square, TMRs, Scatter
 Factors, and other such physics terms ...
- B. And then be able to use them in calculations of accelerator monitorunits

Objectives

- Understand the <u>basic concepts</u> underlying radiation <u>dosimetry</u>
- Recognize the <u>fundamental quantities</u> that are used to describe these basic radiation dosimetry concepts
- Apply radiation dosimetry concepts and quantities in <u>calculations of dose in clinical</u> radiation-oncology practice <u>situations</u>

Clinical Dosimetry

- Fundamental Quantities
 - Think measurements made in a water phantom
 - Define quantities: the ratio of doses at two points: one point different than the other because of distance, depth, and conditions of scatter

MU Calculations

- Apply measured data to clinical dose calculations
- Specifically calculate the monitor-unit setting on the treatment unit that will deliver an intended dose

The next couple of hours

- First talk about how we characterize dose deposition in a medium ... "dosimetry" (dose ratios)
- Then talk about dosecalculation methods ...
 - Perform an accelerator monitor-unit (MU) calculation



Sample Dose Calculation Problem

A patient's whole brain is to be treated.

- The prescribed dose is 300 cGy per fraction, (10 fractions, 30 Gy total dose).
- Radiation and technique are 6 MV x rays, parallelopposed right and left lateral fields
- Prescribed dose is to isocenter.
- Fields are 20x18, mlc-shaped
- The patient set up for isocentric treatment at midbrain, lateral separation 16 cm

A word about the dose prescription

Clearly define the dose prescription:

- Treatment site (e.g. R Lung and mediastinum, L Breast)
- Total dose to the site (including all boost fields)
- Dose per fraction
- Number of fractions
- Fractions per day (and per week)
- Type and energy of radiation (e.g. 6 MV x rays)
- Technique and number of fields (e.g. 9-field IMRT)
- Prescription point, surface, or volume
- Special instructions (e.g. daily kV, bolus)

Who else thinks this is a pretty cool Google Logo?



Beam Data (Measured Dose Ratios)

- Quantitative description of the dose characteristics of the therapy beams
 - All units
 - All energies
- Each machine and energy has its corresponding set of beam data
 - Machine Data Book
- "Golden Data Set"



Varian 2100 6MV Scatter Factors Sc, Sp

				P	erce	nt I	Dept	th D	ose			Fie	ld Siz	e	S.		S,	1		
					V	ariai	1 210	OOC					4		0.951		0.979	6		
6MV PDD Open Unwedged Field								5			0.962		0.983							
field size (cm)	40	50	60	80	80 100 120 150 180 200 220							6			0.975		0.986			
d.max (cm)	1.5	1.5	1.5	1.5	1.5	1.4	14	11	1			8		0 989		0 993				
denth (cm)	4"	Are'	A	4.00	18 18 19 19 19 19 19							10 1.00			1 000		1 000			
1.5	100.0	100.0	100.0	100.0	100.0	100.0	100	0 99.5	99.1	99.	,		12		1 009		1.000			
2.0	98.7	98.8	98.9	98.8	98.9	98.7	98.	98.0	98.	98	1		12		1.000		1.000			
3.0	94.2	94.4	94.5	94.6	94.8	94.8	94 1	8 95 0	94	10 94	7		15		1.021		1.013			
4.0	89.1	89.8	90.0	90.2	90.7	90.6	90	9 91	91	1 91	1		20		1.030		1.023			
5.0	84.2	84.7	85.4	85.8	86.4	86.6	87.	0 87 3	3 87	3 87	4		25		1.038		1.031			
6.0	79.3	80.1	81.0	81.5	82.1	82.7	83	2 83	5 83	6 83	8		30		1.049		1.035			
7.0	74.7	75.7	76.7	77.1	78.1	78.6	79.	3 79.5	9 79	9 80	2		40		1.061		1.040			
8.0	70.5	71.5	72.6	73.2	74.2	74.9	75.	5 76.	2 76	4 76.	7									
9.0	66.5	67.5	68.6	69.3	70.4	71.1	72.	1 72.1	8 73	1 73	4 73	7 74	3 74	7 75	0					
10.0	62.6	63.6	64.6	65.6	8 33	67 5	68	. 03 3	1 03 1	R 70	0 70	4 71	n 71	5 71	8					
11.0	59.0	60.0	61.0	61.						Tiss	ue N	Iax	imu	n R	atio					
12.0	55.5	56.4	57.5	58.	58								2100	10						
13.0	52.1	53.1	54.2	55.								varian 2100 s							10.1.00	11000
14.0	49.1	50.1	51.1	52	SMV	MR					Op	Open Unwedge			Field			1)0cm	SAD
15.0	46.2	47.1	48.1	49.f	ield size	(cm)	4.0	5.0	6.0	8.0	10.0	12.0	15.0	18.0	20.0	22.0	25.0	30.0	35.0	40.0
16.0	43.4	44.4	45.4	46.	d-max (e	(m)	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.2	1.2
17.0	40.9	41.8	42.9	43.	depth (o	:m)														
18.0	38.5	39.4	40.5	41.	1.5		1.000	1.000	1.000	1.000	1.000	1.001	1.001	1.001	1.001	1.001	1.001	1,001	1.001	1.001
19.0	36.3	37.2	38.2	39	2.0		0.996	0.998	0.999	0.999	0.999	0.999	0.998	0.998	0.997	0.997	0.997	0.997	0.997	0.997
20.0	34.2	35.1	35.9	37	3.0		0.96\$	0.971	0.972	0.974	0.976	0.977	0.978	0.979	0.979	0.979	0.980	0.981	0.982	0.983
21.0	32.2	33.1	33.9	35	4.0		0.934	0.939	0.943	0.948	0.951	0.953	0.955	0.957	0.958	0.959	0.960	0.963	0.965	0.967
22.0	30.3	31.2	31.9	33.	5.0		0.897	0.905	0.910	0.918	0.923	0.926	0.930	0.933	0.935	0.937	0.939	0.942	0.946	0.948
23.0	28.7	29.4	30.1	31	6.0		0.\$60	0.870	0.878	0.888	0.895	0.900	0.906	0.910	0.912	0.914	0.917	0.921	0.924	0.928
24.0	27.1	27.8	28.5	29.	7.0		0.825	0.836	0.844	0.857	0.865	0.872	0.879	0.\$\$5	0.555	0.891	0.894	0.899	0.903	0.906
25.0	25.5	26.2	26.9	27.	8.0		0.791	0.804	0.813	0.\$27	0.837	0.\$44	0.853	0.859	0.863	0.866	0.\$71	0.877	0.882	0.\$\$6
26.0	24.1	24.7	25.4	26	9.0		0.759	0.772	0.781	0.796	0.908	0.\$16	0.827	0.\$35	0.839	0.\$43	0.\$49	0.856	0.862	0.\$67

Beam Data: Beam Characteristics

Measured data:

- Statement of calibration
 - How is machine calibrated?
- Percent Depth Dose (PDDs)
 - TMRs are then calculated from PDDs
- Profiles
 - Off-Axis Ratios
- Output Factors
- Transmission Factors
 - Wedges and other attenuators



Beam Data

Percent Depth Dose

Varian 2100C

					Op	100cm SSD											
					Tice		Javi	imu	m P	atio						35.0	40.0
	_				1 122	uc n	1aA	mu		allo						1.2	1.2
						Va	rian	2100	l's								
	6MV TMI	2				Op	en Ui	nwed	10)0cm	99.6	99.6					
	field size (cm)	4.0	5.0	6.0	8.0	10.0	12.0	15.0	18.0	20.0	22.0	25.0	30.0	35.0	40.0	98.2	98.1
	d-max (cm)	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.2	1.2	94.9	95.0
	depth (cm)															91.5	91.6
	1.5	1.000	1.000	1.000	1.000	1.000	1.001	1.001	1.001	1.001	1.001	1.001	1.001	1.001	1.001	04.4	00.2
	2.0	0.996	0.998	0.999	0.999	0.999	0.999	0.998	0.998	0.997	0.997	0.997	0.997	0.997	0.997	04.4	04.7
	3.0	0.968	0.971	0.972	0.974	0.976	0.977	0.978	0.979	0.979	0.979	0.980	0.981	0.982	0.983	77.7	70.0
	4.0	0.934	0.939	0.943	0.948	0.951	0.953	0.955	0.957	0.958	0.959	0.960	0.963	0.965	0.967	747	75.0
	5.0	0.897	0.905	0.910	0.918	0.923	0.926	0.930	0.933	0.935	0.937	0.939	0.942	0.946	0.948	74.1	75.0
	6.0	0.860	0.870	0.878	0.888	0.895	0.900	0.906	0.910	0.912	0.914	0.917	0.921	0.924	0.928	69.4	69.9
	7.0	0.825	0.836	0.844	0.857	0.865	0.872	0.879	0.885	0.888	0.891	0.894	0.899	0.903	0.906	65.4	65.8
	8.0	0.791	0.804	0.813	0.827	0.837	0.844	0.853	0.859	0.863	0.866	0.871	0.877	0.882	0.886	62.6	63.0
	9.0	0.759	0.772	0.781	0.796	0.808	0.816	0.827	0.835	0.839	0.843	0.849	0.856	0.862	0.867	50 0	60.3
Sc, 5	10.0	0.727	0.739	0.750	0.766	0.778	0.788	0.800	0.809	0.814	0.819	0.825	0.833	0.839	0.845	57.2	57.7
	11.0	0.696	0.709	0.719	0.736	0.750	0.760	0.774	0.784	0.790	0.795	0.802	0.811	0.818	0.824	54.6	55.1
	12.0	0.665	0.678	0.689	0.707	0.721	0.732	0.746	0.758	0.764	0.770	0.777	0.787	0.795	0.801	52.1	52.6
	13.0	0.636	0.649	0.660	0.679	0.694	0.706	0.721	0.733	0.740	0.746	0.754	0.764	0.773	0.780	10.8	50.3
	14.0	0.609	0.621	0.632	0.651	0.666	0.679	0.695	0.708	0.716	0.722	0.731	0.742	0.751	0.759	47.5	48.0
	15.0	0.583	0.594	0.605	0.624	0.640	0.653	0.670	0.684	0.691	0.698	0.707	0.719	0.729	0.737	41.5	40.0
	16.0	0.556	0.568	0.579	0.598	0.614	0.628	0.645	0.659	0.667	0.674	0.684	0.697	0.707	0.715	43.3	43.0
	17.0	0.532	0.544	0.555	0.574	0.590	0.604	0.621	0.636	0.644	0.651	0.661	0.674	0.685	0.694	41.2	43.0
	18.0	0.510	0.521	0.531	0.551	0.567	0.581	0.598	0.613	0.621	0.629	0.639	0.653	0.664	0.674	30 /	30.0
	19.0	0.489	0.499	0.509	0.528	0.544	0.558	0.576	0.591	0.600	0.607	0.618	0.632	0.644	0.653	37.5	38.1
	20.0	0.467	0.477	0.487	0.505	0.522	0.536	0.554	0.569	0.578	0.586	0.597	0.611	0.623	0.633	35.7	36.3
	21.0	0.447	0.456	0.466	0.484	0.500	0.515	0.533	0.548	0.557	0.565	0.576	0.591	0.603	0.613	34.1	34.6
	22.0	0.429	0.437	0.446	0.464	0.480	0.494	0.512	0.528	0.537	0.545	0.556	0.571	0.584	0.594	30.0	31 /
	23.0	0.412	0.419	0.427	0.444	0.460	0.474	0.492	0.508	0.517	0.525	0.536	0.552	0.565	0.575	28.1	28.6
	24.0	0.394	0.401	0.409	0.426	0.441	0.455	0.473	0.489	0.498	0.506	0.517	0.533	0.545	0.556	26.1	20.0
	25.0	0.379	0.385	0.392	0.408	0.423	0.437	0.455	0.471	0.480	0.488	0.499	0.515	0.527	0.538	20.0	20.1
	26.0	0.362	0.368	0.375	0.390	0.405	0.419	0.437	0.452	0.461	0.470	0.481	0.496	0.509	0.520	10 1	19.6
	28.0	0.332	0.337	0.344	0.359	0.373	0.386	0.403	0.418	0.427	0.435	0.446	0.462	0.475	0.486	13.1	15.0
	30.0	0.306	0.310	0.316	0.330	0.343	0.356	0.372	0.387	0.395	0.403	0.414	0.430	0.443	0.454		
	32.0	0.280	0.284	0.290	0.303	0.316	0.328	0.344	0.358	0.366	0.374	0.384	0.399	0.412	0.423		
	35.0	0.250	0.253	0.257	0.268	0.280	0.290	0.305	0.319	0.326	0.334	0.344	0.358	0.370	0.381		

What's in the machine data books?

Varian 2100 6MV Scatter Factors Sc.

ield Size	S _c	Sp					
4	0.951	0.979					
5	0.962	0.983					
6	0.975	0.986					
8	0.989	0.993					
10	1.000	1.000					
12	1.008	1.006					
15	1.021	1.013					
20	1.030	1.023					
25	1.038	1.031					
30	1.049	1.035					
40	1.061	1.040					

The Definitions of Field Size

- Many details
 - How defined? ... SSD, SAD
 - Field size at what distance? ...

beam divergence

How produced?
 ... collimator
 jaws, multi-leaf
 collimator







The Definitions of Field Size

Where defined?

- Think ... at what <u>distance</u> is field size defined?
- For S<u>S</u>D geometries
 - Field size defined at <u>surface</u> (e.g. PDD)
- For S<u>A</u>D geometries
 - Field size defined at <u>axis</u> (at depth, e.g. TMR)



Field Size: Equivalent Square

- Data are measured for square fields
- For rectangular or other fields, use ...
- The "equivalent square"
 - Is the size of the square field that produces the <u>same amount of attenuation</u> <u>and scatter</u> (same PDD and OF) as the given field
 - Normally represented by the "side" of the equivalent square

 Table 9.2.

 Equivalent Squares of Rectangular Fields

2	4	6	8	10	12	14	16	18	20	22	24	26	28	30
2.0														-
2.7	4.0													
3.1	4.8	6.0												
3.4	5.4	6.9	8.0											
3.6	5.8	7.5	8.9	10.0										
3.7	6.1	8.0	9.6	10.9	12.0							2		
3.8	6.3	8.4	10.1	11.6	12.9	14.0								
3.9	6.5	8.6	10.5	12.2	13.7	14.9	16.0							
4.0	6.6	8.9	10.8	127	14.3	15.7	16.9	18.0						
4.0	6.7	9.0	11.1	13.0	14.7	16.3	17.7	18.0	20.0					
4.0	6.8	9.1	11.3	13.3	15 1	16.8	18.3	10.0	20.0	22.0				
4.1	6.8	9.2	11.5	13.5	15.4	17.2	18.8	20.3	20.8	22.0	24.0			
4.1	6.9	93	11.6	13 7	15.7	17.5	10.0	20.0	22.4	22.8	24.0			1
41	6.0	9.4	11 7	13.0	15.0	17.9	10.6	20.9	22.4	23.1	24.9	20.0		
4.1	6.9	9.4	11.7	13.9	16.0	18.0	19.9	21.7	23.3	24.4	20.7	27.0	28.0	30
	2 2.0 2.7 3.1 3.4 3.6 3.7 3.8 3.9 4.0 4.0 4.1 4.1 4.1 4.1	2 4 2.0 2.7 4.0 3.1 4.8 3.4 5.4 3.6 5.8 3.7 6.1 3.8 6.3 3.9 6.5 4.0 6.6 4.0 6.7 4.1 6.8 4.1 6.9 4.1 6.9 4.1 6.9	2 4 6 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 3.6 5.8 7.5 3.7 6.1 8.0 3.8 6.3 8.4 3.9 6.5 8.6 4.0 6.6 8.9 4.0 6.7 9.0 4.0 6.8 9.1 4.1 6.8 9.2 4.1 6.9 9.4 4.1 6.9 9.4	2 4 6 8 2.0 2.7 4.0 3.1 4.8 6.0 3.1 4.8 6.9 8.0 3.4 5.4 6.9 8.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 3.7 6.1 8.0 9.6 3.8 6.3 8.4 10.1 3.9 6.5 8.6 10.5 4.0 6.6 8.9 10.8 4.0 6.7 9.0 11.1 4.0 6.8 9.1 11.3 4.1 6.9 9.2 11.5 4.1 6.9 9.3 11.6 4.1 6.9 9.3 11.6 9.4 11.7 4.1 6.9 9.4 11.7 4.1 6.9 9.4 11.7	2 4 6 8 10 2.0 2.7 4.0 3.1 4.8 6.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 3.8 6.3 8.4 10.1 11.6 3.9 6.5 8.6 10.5 12.2 4.0 6.6 8.9 10.8 12.7 4.0 6.6 8.9 10.8 12.7 4.0 6.6 8.9 10.8 12.7 4.0 6.7 9.0 11.1 13.0 4.0 6.6 8.9 10.8 12.7 4.0 6.7 9.0 11.1 13.0 4.1 6.8 9.2 11.5 13.5 13.5 14.1 6.9 9.3 11.6 13.7 4.1 6.9 9.4 11.7 13.8 4.1 6.9 9.4 11.7 <td>2 4 6 8 10 12 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.7 6.1 8.0 9.6 10.9 12.0 3.7 6.1 8.0 9.6 10.9 12.0 3.7 6.1 8.0 9.0 12.0 3.8 6.3 8.4 10.1 11.6 12.9 3.9 6.5 8.6 10.5 12.2 13.7 4.0 6.6 8.9 10.8 12.7 14.3 4.0 6.7 9.0 11.1 13.0 14.7 14.7 13.0 14.7 4.1 6.8 9.1 11.3 13.3 15.1 4.1 4.1 6.9 9.4 11.7 13.8 1</td> <td>2 4 6 8 10 12 14 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 4.0 6.6 8.9 10.8 12.7 14.3 15.7 4.0 6.6 8.9 10.8 12.7 14.3 15.7 4.0 6.6 8.9 10.8 12.7 14.3 15.7 4.0 6.8 9.1 1.3 13.3 15.1 16.8 4.1 6.8 9.2 11.5 13.5 15.4 17.2 4.1 6.9 9.4 11.7 13.8</td> <td>2 4 6 8 10 12 14 16 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 4.0 6.8 9.1 13.5 15.4 1</td> <td>2 4 6 8 10 12 14 16 18 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.4 5.4 6.9 8.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.8 18.3 19.7 4.1 6.8 9.1</td> <td>2 4 6 8 10 12 14 16 18 20 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 10.0 3.7 6.1 8.0 9.6 10.0 3.7 6.1 8.0 9.0 1.0 3.7 6.1 8.0 9.0 1.0 3.7 6.1 8.0 9.0 1.0 3.7 6.1 8.0 9.0 1.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.0 3.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0</td> <td>2 4 6 8 10 12 14 16 18 20 22 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 19.7 20.9 22.0 4.1 6.8 9.1 13.3 15.1</td> <td>2 4 6 8 10 12 14 16 18 20 22 24 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 18.9 20.0 4.1 6.8 9.1 13.3 15.1 16.8 18.3</td> <td>2 4 6 8 10 12 14 16 18 20 22 24 26 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 18.9 20.0 4.1 6.8 9.1 13.3 15.1 16.8 18</td> <td>2 4 6 8 10 12 14 16 18 20 22 24 28 28 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 18.9 20.0 4.1 6.8 9.1 11.5 13.5 15.4 17.2 18.8 20.3 21.7</td>	2 4 6 8 10 12 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.7 6.1 8.0 9.6 10.9 12.0 3.7 6.1 8.0 9.6 10.9 12.0 3.7 6.1 8.0 9.0 12.0 3.8 6.3 8.4 10.1 11.6 12.9 3.9 6.5 8.6 10.5 12.2 13.7 4.0 6.6 8.9 10.8 12.7 14.3 4.0 6.7 9.0 11.1 13.0 14.7 14.7 13.0 14.7 4.1 6.8 9.1 11.3 13.3 15.1 4.1 4.1 6.9 9.4 11.7 13.8 1	2 4 6 8 10 12 14 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 4.0 6.6 8.9 10.8 12.7 14.3 15.7 4.0 6.6 8.9 10.8 12.7 14.3 15.7 4.0 6.6 8.9 10.8 12.7 14.3 15.7 4.0 6.8 9.1 1.3 13.3 15.1 16.8 4.1 6.8 9.2 11.5 13.5 15.4 17.2 4.1 6.9 9.4 11.7 13.8	2 4 6 8 10 12 14 16 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 4.0 6.8 9.1 13.5 15.4 1	2 4 6 8 10 12 14 16 18 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.4 5.4 6.9 8.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.8 18.3 19.7 4.1 6.8 9.1	2 4 6 8 10 12 14 16 18 20 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 10.0 3.7 6.1 8.0 9.6 10.0 3.7 6.1 8.0 9.0 1.0 3.7 6.1 8.0 9.0 1.0 3.7 6.1 8.0 9.0 1.0 3.7 6.1 8.0 9.0 1.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.0 3.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	2 4 6 8 10 12 14 16 18 20 22 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 19.7 20.9 22.0 4.1 6.8 9.1 13.3 15.1	2 4 6 8 10 12 14 16 18 20 22 24 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 18.9 20.0 4.1 6.8 9.1 13.3 15.1 16.8 18.3	2 4 6 8 10 12 14 16 18 20 22 24 26 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 18.9 20.0 4.1 6.8 9.1 13.3 15.1 16.8 18	2 4 6 8 10 12 14 16 18 20 22 24 28 28 2.0 2.7 4.0 3.1 4.8 6.0 3.4 5.4 6.9 8.0 3.6 5.8 7.5 8.9 10.0 3.7 6.1 8.0 9.6 3.7 6.1 8.0 9.6 10.9 12.0 3.8 6.3 8.4 10.1 11.6 12.9 14.0 3.9 6.5 8.6 10.5 12.2 13.7 14.9 16.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.6 8.9 10.8 12.7 14.3 15.7 16.9 18.0 4.0 6.7 9.0 11.1 13.0 14.7 16.3 17.7 18.9 20.0 4.1 6.8 9.1 11.5 13.5 15.4 17.2 18.8 20.3 21.7

From Hospital Physicists' Association. Central axis depth dose data for use in radiotherap Br J Radiol 1978;(suppl 11).

KHAN TABLE 9.2

Rectangular fields are often approximated by square fields having equivalent attenuation and scattering characteristics – the "Equivalent Square". The side, a, of the equivalent square of a rectangular field of length L and width W can be approximated by:



Dose Ratios Concepts: Distance and Depth

Distance

- How far away from the source
 Inverse Square
- Depth
 - How deep in absorber (water, patient)
 - Attenuation
- Note Difference !!
 - Commonly confused



Distance, Depth, and Scatter

- How does the dose at point P differ from that at point Q?
 - Point P farther away
 - Inverse square
 - Point P deeper
 - Attenuation
 - Field size at Point P larger
 - More scatter



1D Dose Distributions

Dosimetry Concepts in 1 Dimension

Percent Depth Dose (PDD)

PDD Notes

- The <u>differences in dose</u> at the two depths, d₀ and d, are due to:
 - Differences in <u>depth</u>
 - Differences in <u>distance</u>
 - Differences in <u>field size</u> at each depth (scatter)
- Field size is defined at the surface of the phantom or patient



 $PDD = D_d / D_{d0}$

PDD: Depth and Energy Dependence

PDD Curves - Characteristics

Note change in depth of d_{max}

 Can characterize beam quality (energy) using PDD at 10-cm depth



PDD Build-up Region

Kerma to dose relationship

- Kerma and dose represent two different quantities
 - Kerma is energy released
 - Dose is energy absorbed
- Build-up region produced by forward-scattered electrons that stop at deeper depths
- Areas under both curves are equal



Figure 9.4. Schematic plot of absorbed dose and kerma as functions of depths

PDD: Distance, Depth, Scatter

Note that in mathematical description of PDD:

Inverse-square (distance) factor

- Dependence on SSD
- Attenuation (depth) factor

Scatter (field-size) factor



PDD: Effect of Distance

- Effect of inverse-square term on PDD
 - <u>As distance increases</u>, relative change in dose rate decreases (less steep slope)
 - Less Inverse-Square effect
 - This results in an <u>increase in</u> <u>PDD</u> (since there is less of a dose decrease due to distance), although the <u>actual dose rate decreases</u>



THE PHYSICS OF RADIATION THERAPY

Percent Depth Dose

	Varian 2100C														
PUU EXAMPLE	6MV PDL				Op	en Ur	wed	ged F	leld			100	cm S	SD	
	field size (cm)	4.0	5.0	6.0	8.0	10.0	12.0	15.0	18.0	20.0	22.0	25.0	30.0	35.0	40.0
	d-max (cm)	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.2	1.2	1.2
	depth (cm)														
	1.5	100.0	100.0	100.0	100.0	100.0	100.0	100.0	99.9	99.7	99.7	99.7	99.5	99.6	99.6
	2.0	98.7	98.8	98.9	98.8	98.9	98.7	98.7	98.6	98.4	98.4	98.3	98.3	98.2	98.1
If the dose in a 10x10	cm [*] ti	iëto	89.8	90.0	94.6	94.8	94.8 90.6	94.8	95.0 91.1	94.9 91.1	94.7 91.1	94.8 91.2	94.9 91.4	94.9 91.5	95.0 91.6
	5.0	84.2	84.7	85.4	85.8	86.4	86.6	87.0	87.3	87.3	87.4	87.6	87.8	88.0	88.2
the depth of d _{max} in wo	ater I (JU	6h	81.0	81.5	82.1	82.7	83.2	83.6	83.6	83.8	84.0	84.3	84.4	84.7
	7.0	74.7	75.7	76.7	77.1	78.1	78.6	79.3	79.9	79.9	80.2	80.5	80.7	81.0	81.3
SDD is 200 cGv. what	is the	đó	s ⁷ é	72.6	73.2	74.2	74.9	75.6	76.2	76.4	76.7	77.1	77.5	77.7	78.2
	9.0	66.5	67.5	68.6	69.3	70.4	71.1	72.1	72.8	73.1	73.4	73.7	74.3	74.7	75.0
at a depth of 10 cm ²	10.0	62.6	63.6	64.6	65.6	66.8	67.5	68.6	69.4	69.8	70.0	70.4	71.0	71.5	71.8
	11.0	59.0	60.0	61.0	61.9	63.2	64.2	65.3	66.2	66.5	66.9	67.3	68.0	68.4	68.8
	12.0	55.5	56.4	57.5	58.5	59.9	60.8	62.1	62.9	63.4	63.8	64.3	64.9	65.4	65.8
	13.0	52.1	53.1	54.2	55.3	50.0	51.0	59.0	59.9	60.4	60.9 E0.0	61.3 50 5	62.0	62.6	63.0
	14.0	49.1	17 1	18 1	19.3	50.7	54.0	53.2	5/ 2	54.7	55.3	55.8	56.5	57.2	60.5 57.7
$PDD = D_d / D_{d0}$	16.0	43.4	44 4	45.4	46.5	48.0	49 1	50.5	51.5	52.0	52.6	53.2	53.9	54 6	55 1
	17.0	40.9	41.8	42.9	43.9	45.4	46.5	48.0	48.9	49.4	50.0	50.7	51.5	52.1	52.6
	18.0	38.5	39.4	40.5	41.5	42.9	44.1	45.5	46.5	47.0	47.6	48.3	49.1	49.8	50.3
$D_d = D_{d0} \times PDD$	19.0	36.3	37.2	38.2	39.2	40.6	41.8	43.2	44.2	44.7	45.3	46.0	46.8	47.5	48.0
	20.0	34.2	35.1	35.9	37.0	38.4	39.5	41.0	42.0	42.6	43.1	43.8	44.6	45.3	45.8
	21.0	32.2	33.1	33.9	35.0	36.3	37.5	38.8	39.9	40.4	41.0	41.7	42.5	43.2	43.8
$D_d = 200 \times 0.668 = 133.6$	22.0	30.3	31.2	31.9	33.0	34.4	35.5	36.8	37.9	38.4	39.0	39.7	40.5	41.3	41.8
	23.0	28.7	29.4	30.1	31.2	32.5	33.6	34.9	36.0	36.5	37.1	37.8	38.6	39.4	39.9
	24.0	27.1	27.8	28.5	29.5	30.8	31.9	33.1	34.2	34.8	35.3	36.0	36.8	37.5	38.1
	25.0	25.5	26.2	26.9	27.9	29.1	30.1	31.4	32.5	33.1	33.6	34.2	35.1	35.7	30.3
	28.0	24.1	24.1	22.4	23.6	24.7	25.6	26.8	27.8	28.3	28.9	29.5	30.3	30.9	314
	30.0	19.1	19.7	20.3	21.1	22.1	23.0	24.1	25.1	25.6	26.1	26.7	27.5	28.1	28.6
	32.0	17.0	17.6	18.1	18.9	19.9	20.7	21.7	22.6	23.2	23.6	24.2	24.9	25.5	26.1
	35.0	14.4	14.9	15.3	16.1	16.9	17.7	18.6	19.5	19.9	20.3	20.9	21.6	22.1	22.5
	38.0	12.2	12.6	13.0	13.6	14.4	15.1	15.9	16.7	17.1	17.5	18.0	18.6	19.1	19.6

The Mayneord F Factor (no longer a mystery)

- The inverse-square term within the PDD
 - PDD is a function of distance (<u>SSD</u> + depth)
 - PDDs at given depths and distances (SSD) can be corrected to produce approximate PDDs at the same depth but at other distances by applying the Mayneord F factor
 - "Divide out" the previous inverse-square term (for SSD₁), "multiply in" the new inverse-square term (for SSD₂)



The Mayneord F Factor

- Mayneord F Example
- Previous Problem
 - 100 SSD, 10x10, depth 10
 - PDD was 0.668
- Now assume 120 SSD ...
- Divide out 100 SSD, d₁₀ inverse square, and multiply back in 120 SSD, d₁₀ inverse square:

$$\begin{bmatrix} (21.5/2)^{2} \\ 130/(01.5/2)^{2} \\ 110/ \end{bmatrix} \times 0.668 = 0.685$$

$$F = \left\{ \frac{SSD_2 + d_{\max}}{SSD_2 + d} \right\}^2$$



TAR: A traditional yet useful quantity

□ The TAR ...

- Developed for isocentric treatments
- The ratio of doses at two points:
- Equidistant from the source
 - That have <u>equal field sizes</u> at the points of calculation
 - Field size is defined at point of calculation
- Relates dose at depth to dose "in air" (free space)
 - Concept of "equilibrium mass"
 - Need for electronic equilibrium – constant Kerma-to-dose relationship



 $TAR = D_d / D_{fs}$

PSF (BSF): An extension of the TAR

- The PSF (or BSF) is a special case of the TAR when dose in air is compared to dose at the depth (d_{max}) of maximum dose
 - At this point the dose is maximum (peak) since the contribution of scatter is not offset by attenuation
- The term BSF applies strictly to situations where the depth of d_{max} occurs at the surface of the phantom or patient (i.e. kV x rays)



PSF Details: Energy and Field Size

 In general, scatter contribution decreases as energy increases

Note:

- Scatter can contribute as much as 50% to the dose a d_{max} in kV beams
- The effect at ⁶⁰Co is of the order of a few percent (PSF ⁶⁰Co 10x10 = 1.035
- Increase in dose is greatest in smaller fields (note 5x5, 10x10, and 20x20)



TPR and TMR: More current quantities

- Similar to the TAR, the TPR is the ratio of doses (D_d and D_{t0}) at two points equidistant from the source
 - Field sizes are equal
 - Again field size is defined at depth of calculation
 - Only attenuation by depth differs
- The TMR is a special case of the TPR when t₀ equals the depth of d_{max}



 $TPR = D_d / D_{t0}$

TMR (and PDD) vs. Field Size: Scatter contribution vs. field size

- The TMR (or TAR or PDD) for a given depth can be plotted as a function of field size
 - Shown here are TMRs at 1.5, 5.0, 10.0, 15.0, 20.0, 25.0, and 30.0 cm depths as a function of field size
- Note the lesser increase in TMR as a function of field size
 - This implies that differences in scatter are of greater significance in smaller fields than larger fields,



TMR / PDD / TAR Relationships



Fig. 2.1 Diagram illustrating relationships between absorbed doses used in forming percentage depth dose, tissue-air ratio and tissue-phantom ratio. All three radiation beams are identical except that the one on the left irradiates air only while the other two irradiate a water phantom. Tissue-air ratio, T, is the absorbed dose at a point such as X divided by that at X'. Percentage depth dose, P, is the absorbed dose at X divided by that at Y, expressed as a percentage. Tissue-phantom ratio, T_P , is the absorbed dose at X divided by that at Y divided by that at X'. To is the tissue-air ratio at the depth of the peak absorbed dose and I is the inverse square relationship.

From: ICRU 14

TMR / PDD Relationship



Scatter Factors

- Characterize scatter
- Scatter factors describe field-size dependence of dose at a point
 - Often wise to separate sources of scatter
 - Scatter from the head of the treatment unit
 - Scatter from the phantom or patient
 - Measurements complicated by need for electronic equilibrium



Figure 10.1. Arrangement for measuring S_c and $S_{c,p}$. **A**, Chamber with build-up cap in air to measure output relative to a reference field, for determining S_c versus field size. **B**, Measurements in a phantom at a fixed depth for determining $S_{c,p}$ versus field size. Reprinted with permission from Khan FM, Sewchand W, Lee J, Williamson JF. Revision of tissue-maximum ratio and scatter-maximum ratio concepts for cobalt 60 and higher energy x-ray beams. Measurements 1980;7:230.

 S_c = collimator scatter factor S_p = phantom scatter factor

Transmission Factors: Wedges

- Beam intensity is also affected by the introduction of beam attenuators that may be used modify the beam's shape or intensity
 - Such attenuators may be plastic trays used to support field-shaping blocks, or physical wedges used to modify the beam's intensity
- The transmission of radiation through attenuators is often fieldsize and <u>depth dependent</u>
 - Wedged field PDDs

Wedge Transmission Factors

Dependence on Depth and Field Size

Varian Clinac 2100C SN 241 MUSC 11/12/98



The Dynamic Wedge

- Wedged dose distributions can be produced without physical attenuators
 - With "dynamic wedges", a wedged dose distribution is produced by sweeping a collimator jaw across the field duration irradiation
 - The position of the jaw as a function of beam irradiation (monitor-unit setting) is given the wedge's "segmented treatment table (STT)
 - The STT relates jaw position to fraction of total monitor-unit setting



Gibbons
Off-Axis Quantities

- To a large degree, quantities and concepts discussed up to this point have addressed dose along the "central axis" of the beam
- It is necessary to characterize beam intensity "off-axis"
 - Two equivalent quantities are used
 - Off-Axis Factors (OAF)
 - Off-Center Ratios (OCR)
 - These two quantities are equivalent



 $OAF(x,d) = D_{d,x}/D_{d,0}$

where x = distance off-axis

Off-Axis Factors: Measured Profiles

- Off-axis factors are extracted from measured profiles
 - Profiles are smoothed, may be "symmetrized", and are normalized to the central axis intensity



Off-Axis Factors: Typical Representations

- OAFs (OCRs) are often tabulated and plotted versus depth as a function of distance off axis
 - Where "distance off axis" means radial distance away from the central axis
 - Note that, due to beam divergence, this distance varies with distance from the source

Depth		Off-Axis "Tangent"										
(0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.10			
	Off Axis Distance (at 100 cm field-size definition distance)											
0	0	+	2	3	4	5	6	8	10			
1.7	1.000	1.007	1.012	1.020	1.028	1.035	1.040	1.046	1.051			
5	1.000	1.009	1.016	1.023	1.030	1.035	1.037	1.041	1.045			
10	1.000	1.007	1.013	1.020	1.024	1.024	1.025	1.025	1.024			
15	1.000	1.001	1.007	1.011	1.015	1.016	1.015	1.011	1.003			
20	1.000	1.003	1.007	1.011	1.012	1.014	1.009	1.001	0.988			
25	1.000	1.003	1.005	1.005	1.006	1.007	1.001	0.986	0.971			
30	1.000	1.004	1.006	1.008	1.008	1.006	0.998	0.981	0.963			



Off-Axis Wedge Corrections

- Descriptions vary of off-axis intensity in wedged fields
 - Measured profiles contain both open-field off-axis intensity as well as differential wedge transmission
 - We have defined off-axis wedge corrections as corrections to the central axis wedge factor
 - Open-field off-axis intensity is divided out of the profile
 - The corrected profile is normalized to the central axis value

		Distance Off-Axis	15 Wedge OAWC	30 Wedge OAWC	45 Wedge OAWC	60 Wedge OAWC	
1	Тое	-6.000	1.066	1.200	1.343	1.597	
Ι		-5.000	1.048	1.159	1.275	1.485	
/		-4.000	1.036	1.124	1.212	1.379	
- 11		-3.500	1.030	1.108	1.181	1.323	
- /		-3.000	1.025	1.092	1.155	1.273	
- /		-2.500	1.024	1.076	1.127	1.220	
		-2.000	1.013	1.059	1.104	1.171	
		-1.500	1.015	1.042	1.074	1.125	
		-1.000	1.010	1.027	1.051	1.075	
		-0.500	1.008	1.018	1.032	1.047	_
		0.000	1.000	1.000	1.000	1.000	\sim
1 1		0.500	0.997	0.988	0.980	0.958	
1		1.000	0.980	0.976	0.953	0.922	
		1.500	0.971	0.957	0.924	0.881	
		2.000	0.960	0.938	0.903	0.847	
		2.500	0.949	0.924	0.891	0.814	
		3.000	0.942	0.904	0.875	0.779	
		3.500	0.935	0.899	0.843	0.750	
-		4.000	0.929	0.884	0.823	0.716	
		5.000	0.923	0.855	0.785	0.664	
	Heel	6.000	0.906	0.837	0.744	0.607	

Off-Axis Distance defined at the isocenter

Dose Ratios: What have we learned

- PDDs and TMRs
 - One has inverse square and the other does not
- Field Size
 - At what distance
 - Equivalent square
- Scatter Factors
 - From accelerator head
 - From phantom (patient)

□ Almost halfway there ...





Combine 1D Dosimetry Concepts

Family of Beam Profiles

- Consider beam profiles acquired at multiple depths
- Can combine these profiles with a centralaxis PDD scan to produce a series of "isodose curves"



Figure 11-1 Graphic representation of several measured beam profiles of the type often entered into a treatment planning computer. The illustration shows a number of profiles made along lines perpendicular to the central axis at several depths in a water phantom.

Isodose Curves

- Isodose curves are "lines" connecting equal intensities or doses
 - Commonly normalized to d_{max} along central axis
- Characteristics
 - Flatness
 - Penumbra
 - Penetration
 - Depth of Dose Maximum



Wedged-field Isodose Distribution

- Wedge angle defined at
 - Depth of 80% (old definition)
 - At 10 cm depth (new IEC definition)
- Distribution can be normalized to d_{max} central axis of wedged field
 - Sometimes normalized to open field



Isodose Curve Summation: Parallel Opposed Fields



Hourglass Shape

Parallel Opposed Fields



Figure 11.10. Composite isodose distribution for a pair of parallel opposed fields. A, Each beam is given a weight of 100 at the depth of D_{max} . B, isocentric plan with each beam weighted 100 at the isocenter.

What are percent doses at midplane and at exit?

Two Pairs of Parallel Opposed Fields

- Using two pairs of parallel opposed fields at 90 degrees to each other results in peripheral doses on the order of only 60-70 percent of the isocenter dose
- □ The four-field box



Three Field Beam Arrangement

- Increased avoidance of critical structures can also be achieved using a three field technique
- Three fields can introduce challenges into daily setup, however:
 - Table rail obstruction for beam entry
 - Center spine obstruction for port filming



Combinations of Wedged Fields



Figure 8-14 Diagram showing isodose distribution of various treatment techniques from T1 glottic carcinoma. (See text for optimal plans.)

Penumbrae

Physical Penumbra

- Is the region of the beam not irradiated by entire source
 - Accelerator source diameter is about 2 mm
- Depends on source size, distance from the source to beam-definition device, and distance from source to measurement plane





Penumbrae

- Penumbrae of radiation beams include scatter as well as physical characteristics
 - Common definition is distance between 80% and 20% isodose
 - Typical (corrected *) penumbrae depend on energy, and depth
 - **3-6 mm 80%-20%**
 - * corrected for detector response



Schinkel, and others ...

A "Physics Joke" ...



Intermission

- Take a <u>brief</u> break
 - Don't go too far!
 - Stand up
 - □ Stretch
 - □ Is this OK ... ??
- "Dose Calculations" is next



Dose Calculations

Calculation of linear accelerator monitor-unit (MU) settings to deliver a prescribed dose

Problems



Our Sample Problem

□ A patient's whole brain is to be treated.

- The prescribed dose is 30 Gy total dose, 300 cGy per fraction, 10 fractions, 5 fractions per week. Radiation and technique are 6 MV x rays, parallelopposed right and left lateral fields; prescribed dose is to isocenter.
- Fields are 20x18, mlc-shaped
- The patient set up for isocentric treatment at midbrain, lateral separation 16 cm

First rule of dose calcs ...



Make a picture

Now ... let's reason this through ..

Output: From Relative Dose Ratios to Absolute Dose

Standard calibration geometry

- The geometry used to determine the dose output of the treatment unit
 - Treatment units are calibrated such that their absolute dose is known at a single point (the calibration point) in a predetermined (standard) geometry
 - Calibration geometries are SAD Calibration and SSD Calibration



Introduction

Standard calibration point and geometry (SAD)

- For linear accelerators in the Department of Radiation Oncology, University of Maryland School of Medicine, and commonly elsewhere, this point is located at d_{max} in a water phantom, 100 cm SAD, along the central axis of an open 10x10 field.
- The unit is calibrated such that <u>a dose equal to 1.0 cGy</u> is delivered to this point <u>per 1 Monitor Unit (MU)</u> setting

Introduction

Standard calibration geometry (SSD)

- Other radiation oncology centers, UT M.D. Anderson Cancer Center for example, use an SSD calibration geometry
- At these centers, this point is located at d_{max} in a water phantom, 100 cm SSD, along the central axis of an open standard field, most commonly the 10x10 field.
- At this point (note farther from the source), the unit is calibrated such that 1 monitor unit (MU) is equal to 1.0 cGy

Introduction

Corrections to standard geometry

- At depths other than d_{max}, distances other than the standard SAD or SSD, and for field sizes other 10x10, and points off of the central axis, corrections become necessary
 - Depth corrections are PPDs or TMRs,
 - Distance corrections are Inverse-Square corrections, and
 - Field-size corrections are Scatter Factors.
 - Corrections for points <u>away from the central axis</u> of the beam are Off-Axis Factors
 - <u>Corrections</u> are also necessary to account <u>for transmission through</u> <u>beam attenuators</u> such as wedges
 - These corrections are given in tabulated beam data where relationships to the standard geometry have been established

Corrections to standard geometry: Summary

- Depth corrections
- □ Field-size corrections

Distance corrections

- PDD, TAR, TMR
- Output (scatter factors)
 S_T S_P S_C
- Inv. Sq.
 "SAD" or "SSD" Factors

- Off-axis corrections
- Attenuation corrections

WFs, TFs, etc.

Formalism

In general, the dose (D) at any point in a water phantom can be calculated using the following formalism:

$D = MU \times O \times OF \times ISq \times DDF \times OAF \times TF$

where:

- \blacksquare *MU* = monitor-unit setting
- O = calibrated output (cGy/MU)
- OF = output (scatter) factor(s): S_C , and S_P , or S_T
- ISq = inverse-square correction of output (as needed)
- DDF = depth-dose factors (PDD, TMR, or TAR)
- OAF = off-axis factors
- TF = transmission factors

SAD Beams / SAD Calibration

When the treatment unit is calibrated in a "SAD" geometry, then for "SAD" (isocentric) beams, the formalism becomes:

$D = MU \times S_C \times S_P \times TMR \times OAF \times TF$

- where it is assumed that **output (scatter) factors are given by S_C and** S_{p} , and where it is also assumed that the **calibrated output = 1.0** cGy/MU at the SAD.
- Note that no inverse-square term is needed since the distance to the point of <u>dose normalization</u> is equal to the distance to the point of <u>dose</u> <u>calibration</u> (i.e. both the point of dose normalization and the point at which output is defined are the same).

SSD Beams / SAD Calibration

When the treatment unit is calibrated in a "SAD" geometry, then for "SSD" beam calculations, the formalism becomes:

$D = MU \times S_C \times S_P \times PDD \times ISq \times OAF \times TF$

where the inverse-square factor accounts for the change in output produced by the differences in the distances between the <u>source</u> and the point of <u>calibration (SCD)</u> and between the <u>source</u> and the <u>point of normalization (SPD)</u>

$$ISq = \left(\frac{CD}{SPD} \right)^{2}$$

Formalism Notes: Inverse Square

- The inverse-square term of the SSD Beams / SAD Calibration equation accounts for the decreased output that exists at the increased SSD + d_{max} distance relative to the output that exists at isocenter (where the machine output is 1 cGy/MU).
 - Since the point of dose normalization (SSD + d_{max}) is further away from the source than is the point of dose definition (isocenter), the inverse square term is a factor < 1.0
 - For SAD = 100 cm treatment units, and 6 MV x rays, this inversesquare term is:

$$ISq = F_{SAD} \rightarrow SSD = \left(\frac{CD}{SPD} \right)^{2} = \left(\frac{00}{100 + 1.5} \right)^{2} = 0.971$$

Note that this inverse square term corrects the treatment-unit's dose output

SSD Beams / SSD Calibration

When the treatment unit is calibrated in a "SSD" geometry, then for "SSD" beams, the formalism becomes:

$D = MU \times S_C \times S_P \times PDD \times OAF \times TF$

■ Again, note that no inverse-square term is needed since the distance to the point of <u>dose normalization</u> (SSD + d_{max}) is equal to the distance to the point of <u>dose calibration</u>.

SAD Beams / SSD Calibration

When the treatment unit is calibrated in a "SSD" geometry, then for "SAD" (isocentric) beams, the formalism becomes:

$D = MU \times S_C \times S_P \times ISq \times TMR \times OAF \times TF$

where again the inverse-square factor accounts for the change in output produced by the differences in the distances between the <u>source</u> and the point of <u>c</u>alibration (SCD) and between the <u>s</u>ource and the <u>p</u>oint of normalization (SPD):

$$ISq = \left(\frac{CD}{SPD} \right)^{2}$$

The inverse-square correction in this case is a factor > 1.0, since isocenter is closer to the source than is 100 SSD + dmax.

Formalism Notes: Field Sizes

- Field sizes, unless otherwise stated, represent collimator settings
 - For most accelerators, field sizes are defined at 100 cm (the distance from the source to isocenter)
 - For SSD beams, field sizes are defined at the surface (normally 100 cm SSD)
 - For SAD beams, field sizes are defined at the depth of dose calculation (normally 100 cm SAD)
 - For field sizes at distances other than 100 cm, field sizes must be computed using triangulation:

$$FS_{SSD, d} = FS_{100} \times (SD + d/100)$$

Formalism Notes: Field Size Details

Scatter Factors, PDDs, TMRs

 \square S_C is a function of the collimator setting

 \square S_P is a function of the size of the field:

at the phantom surface for SSD beams

at the depth of calculation for SAD beams

PDDs are a function of:

field size at the phantom surface (SSD beams)

TMRs are a function of:

field size at depth (SAD beams)

Formalism Notes: Prescribed Dose

- In general, one wishes to compute the MU setting necessary to deliver a certain dose to a defined point.
 - This dose is "prescribed", and
 - Its value must be known at the point of calculation.
- When fields are <u>combined</u> to produce a prescribed dose at a point, the doses from each field are computed from the relative weights of each field.
 - Thus, if a dose D_{Rx} is prescribed through multiple fields *i* each having a relative weight wt_i , then the dose D_i from each field is:

$$D_i = D_{Rx} \times \left(\underbrace{Wt_i}_{i} \underbrace{\sum_{i} Wt}_{i} \right)$$
Formalism: Summary

For SAD beams and SAD calibration:

 $MU_i = \frac{D_i}{S_C \times S_P \times TMR \times OAF \times TF}$

For SSD beams and SAD calibration:

 $MU_{i} = \frac{D_{i}}{S_{C} \times S_{P} \times ISq \times PDD \times OAF \times TF}$

Back to our Sample Problem ...

□ A patient's whole brain is to be treated.

- The prescribed dose is 30 Gy total dose, 300 cGy per fraction, 10 fractions, 5 fractions per week. Radiation and technique are 6 MV x rays, parallelopposed right and left lateral fields; prescribed dose is to isocenter.
- Fields are 20x18, mlc-shaped
- The patient set up for isocentric treatment at midbrain, lateral separation 16 cm

Sample Problem

 First compute equivalent squares of the fields:

$$EqSq = \langle LW / L + W \rangle = \langle 20 \times 18 / 20 + 18 \rangle = 19.0$$

Then look up Output Factors and TMRs

•
$$FS = 19 \text{ cm}^2$$
 Depth = 8 cm

Substitute in:

$$MU = \frac{Dose}{S_C \times S_P \times TMR \times OAF \times TF}$$

Assumes SAD Calibration

□ And you're done!

6MV TMR					Open Unwedged Field				
ield size (cm)	4.0	5.0	6.0	8.0	10.0	12.0	15.0	18.0	20.0
d-max (cm)	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.3
depth (cm)									
1.5	1.000	1.000	1.000	1.000	1.000	1.001	1.001	1.001	1.001
2.0	0.996	0.998	0.999	0.999	0.999	0.999	0.998	0.998	0.997
3.0	0.968	0.971	0.972	0.974	0.976	0.977	0.978	0.979	0.979
4.0	0.934	0.939	0.943	0.948	0.951	0.953	0.955	0.957	0.958
5.0	0.897	0.905	0.910	0.918	0.923	0.926	0.930	0.933	0.935
6.0	0.860	0.870	0.878	0.888	0.895	0.900	0.906	0.910	0.912
7.0	0.825	0.836	0.844	0.857	0.865	0.872	0.879	0.885	0.888
8.0	0.791	0.804	0.813	0.827	0.837	0.844	0.853	0.859	0.863



Thank You!

Clinical Dosimetry

